

## SCOTSMAN ICE SYSTEM

### HID312 ICE MACHINE (COUNTERTOP MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/13/15**

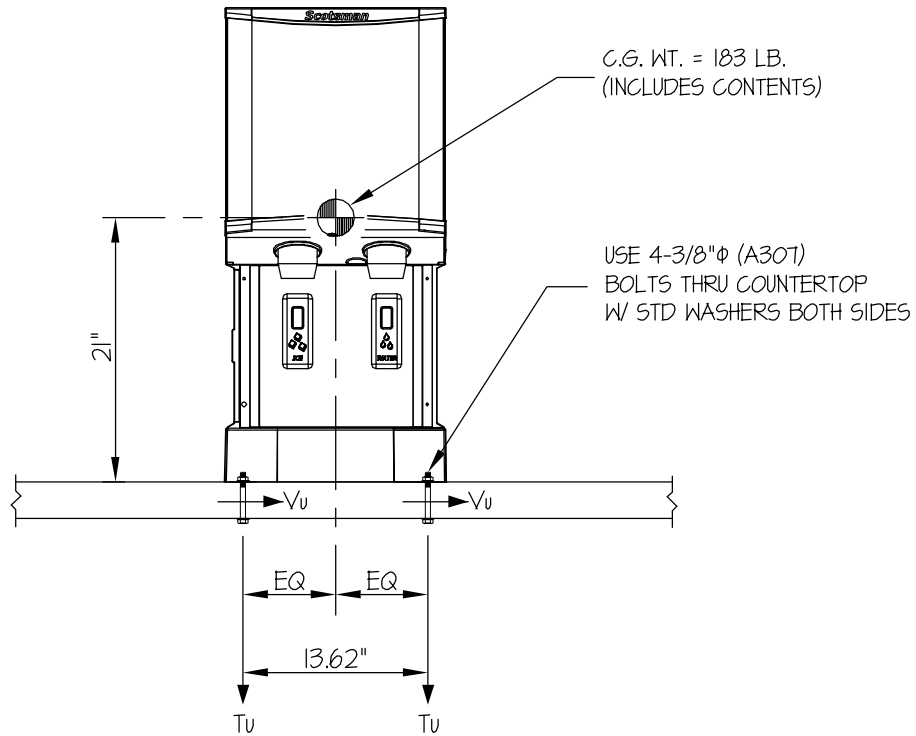
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



$T_u$  = 291 LB/BOLT (MAX)  
 $V_u$  = 82 LB/BOLT (MAX)

#### FRONT ELEVATION

#### NOTES:

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10  
STRENGTH DESIGN IS USED. ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )  
HORIZONTAL FORCE ( $E_h$ ) =  $1.58 W_p$   
VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN.  
THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE  
DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER  
LOADS THAT MAY BE PRESENT.



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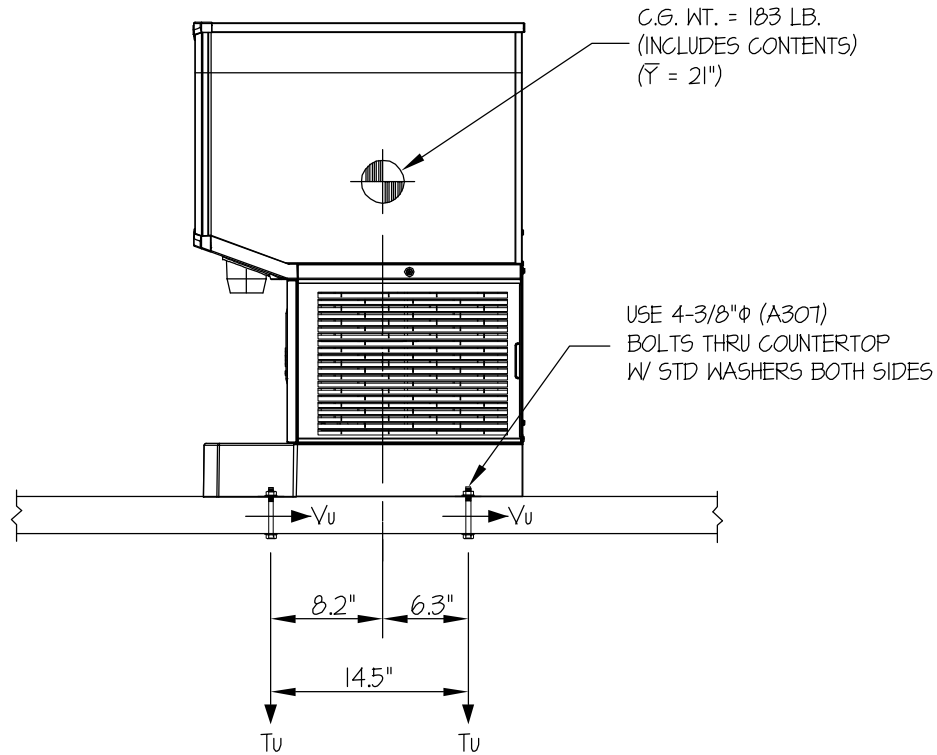
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



**SIDE ELEVATION**

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 183 LB

HORIZONTAL FORCE ( $E_h$ ) =  $1.58W_p = 289$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.44W_p = 81$  LB

BOLT FORCES:

TENSION (T)

$$T_u \text{ MAXIMUM} = \left[ \frac{289\#(21")}{2 \text{ BOLTS}(14.5")} \times (0.3) \right] + \frac{289\#(21")(8.2")}{2 \text{ BOLTS}(13.62")(14.5")} - \frac{(183\#(0.9) - 81\#)(8.2")}{2 \text{ BOLTS}(14.5")} = 291 \text{ LB/BOLT (MAX)}$$

( HORIZ - FRONT TO BACK )                      ( HORIZ - SIDE TO SIDE )                      ( 0.9WEIGHT) -  $E_v$

SHEAR (V)

$$V_u \text{ MAXIMUM} = \frac{289\#(8.2")}{2 \text{ BOLTS}(14.5")} = 82 \text{ LB/BOLT (MAX)}$$

BOLT SPEC: 3/8"  $\phi$  (A307) BOLTS

$\phi T = 3355$  LB/BOLT

$\phi V = 1723$  LB/BOLT

## SCOTSMAN ICE SYSTEM

### HID312 ICE MACHINE (WALL MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/13/15**

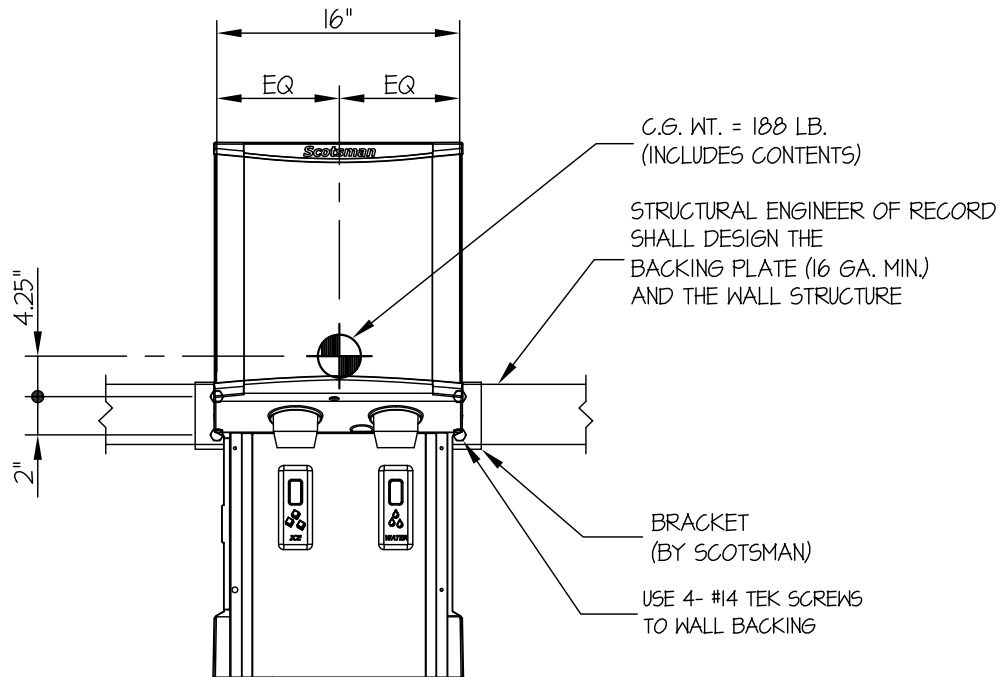
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED

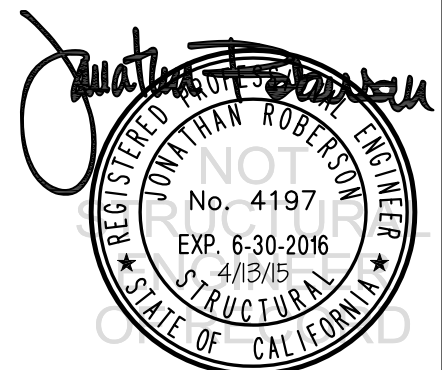


$T_u = 237$  LB/SCREW (MAX)  
 $V_u = 107$  LB/SCREW (MAX)

FRONT ELEVATION

NOTES:

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10**  
STRENGTH DESIGN IS USED. ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )  
HORIZONTAL FORCE ( $E_h$ ) =  $1.58 W_p$   
VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



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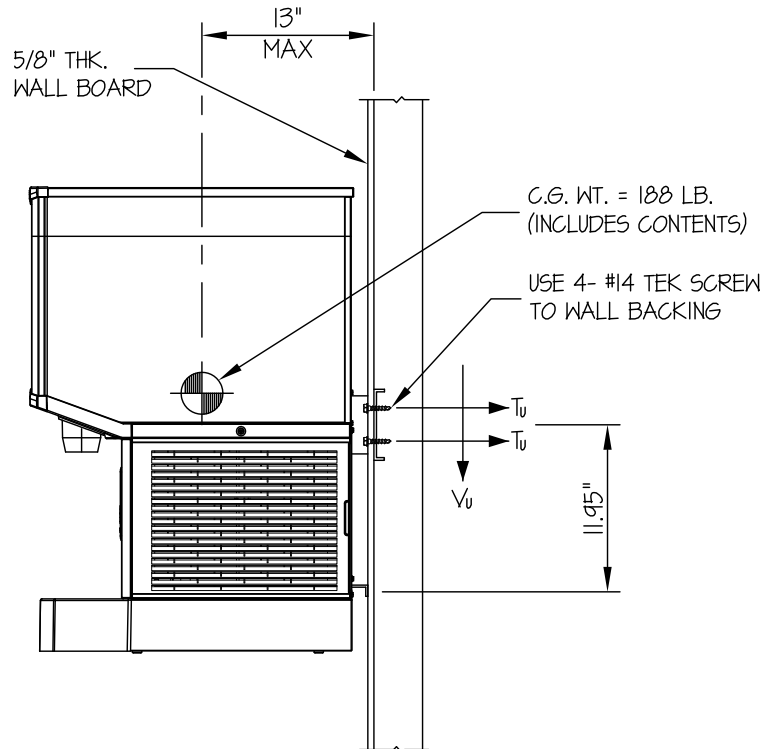
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



### STEEL STUD WALL SECTION

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 188 LB

HORIZONTAL FORCE ( $E_h$ ) =  $1.58W_p = 297$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.44W_p = 83$  LB

BOLT FORCES:

TENSION (T)

$$T_{U \text{ VERTICAL}} = \frac{(188\#)(1.2) + 83\#(13'')}{4 \text{ SCREWS}(11.95'')} = 84 \text{ LB/SCREW}$$

$$T_{U \text{ PARALLEL}} = \frac{297\#(13'')}{2 \text{ SCREWS}(16'')} = 121 \text{ LB/SCREW}$$

$$T_{U \text{ PERP.}} = \frac{297\#(17.2'')}{4 \text{ SCREWS}(11.95'')} = 107 \text{ LB/SCREW}$$

$$T_{U \text{ MAX}} = 84\# + 121\# + 0.3(107\#) = 237 \text{ LB/SCREW (MAX)}$$

SHEAR (V)

$$V_{U \text{ MAX}} = \sqrt{\left(\frac{(1.2(188\#) + 83\#)}{4 \text{ SCREWS}}\right)^2 + \left(\frac{297\#}{4 \text{ SCREWS}}\right)^2} = 107 \text{ LB/SCREW (MAX)}$$

#14 TEK SCREWS TO 16 GAGE, 50 KSI

$\phi T = 418$  LB/SCREW (TENSION)

$\phi V = 362$  LB/SCREW (SHEAR)

## SCOTSMAN ICE SYSTEM

### HID525 ICE MACHINE (COUNTERTOP MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/13/15**

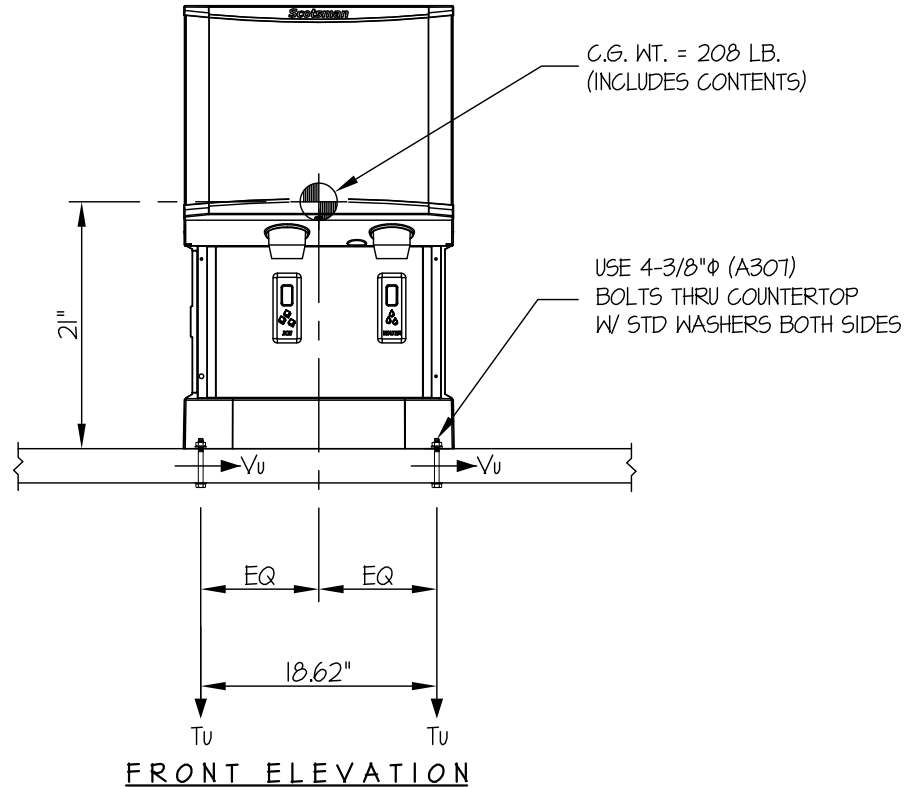
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



T<sub>u</sub> = 274 LB/BOLT (MAX)  
V<sub>u</sub> = 93 LB/BOLT (MAX)

**NOTES:**

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10**  
STRENGTH DESIGN IS USED. ( $S_{ds} = 2.20$ ,  $a_p = 10$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )  
HORIZONTAL FORCE ( $E_h$ ) =  $1.58 W_p$   
VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
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## SCOTSMAN ICE SYSTEM

### HID525 ICE MACHINE (COUNTERTOP MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/13/15**

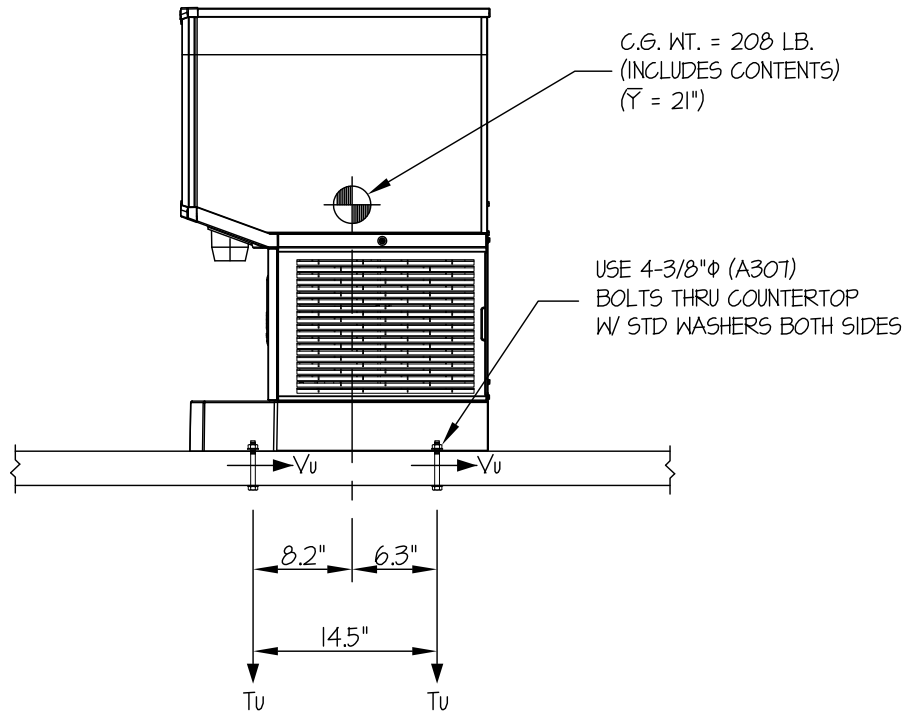
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



SIDE ELEVATION

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED ( $S_{Ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 208 LB

HORIZONTAL FORCE ( $E_h$ ) =  $1.58W_p = 329$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.44W_p = 92$  LB

BOLT FORCES:

BOLT SPEC: 3/8" phi (A307) BOLTS

$\phi T = 3355$  LB/BOLT

$\phi V = 1723$  LB/BOLT

TENSION (T)

$$T_{U \text{ MAXIMUM}} = \left[ \frac{329\#(21\")(8.2\"){}}{1 \text{ BOLT } (18.62\")(14.5\")} \times (0.3) \right] + \frac{329\#(21\"){}}{2 \text{ BOLTS } (14.5\")} - \frac{(208\#(0.9) - 92\#)(8.2\"){}}{2 \text{ BOLTS } (14.5\")} = 274 \text{ LB/BOLT (MAX)}$$

( HORIZ - SIDE TO SIDE )                      ( HORIZ - FRONT TO BACK )                      ( 0.9WEIGHT) -  $E_v$

SHEAR (V)

$$V_{U \text{ MAXIMUM}} = \frac{329\#(8.2\"){}}{2 \text{ BOLTS } (14.5\")} = 93 \text{ LB/BOLT (MAX)}$$

## SCOTSMAN ICE SYSTEM

### HID525 ICE MACHINE (WALL MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/22/15**

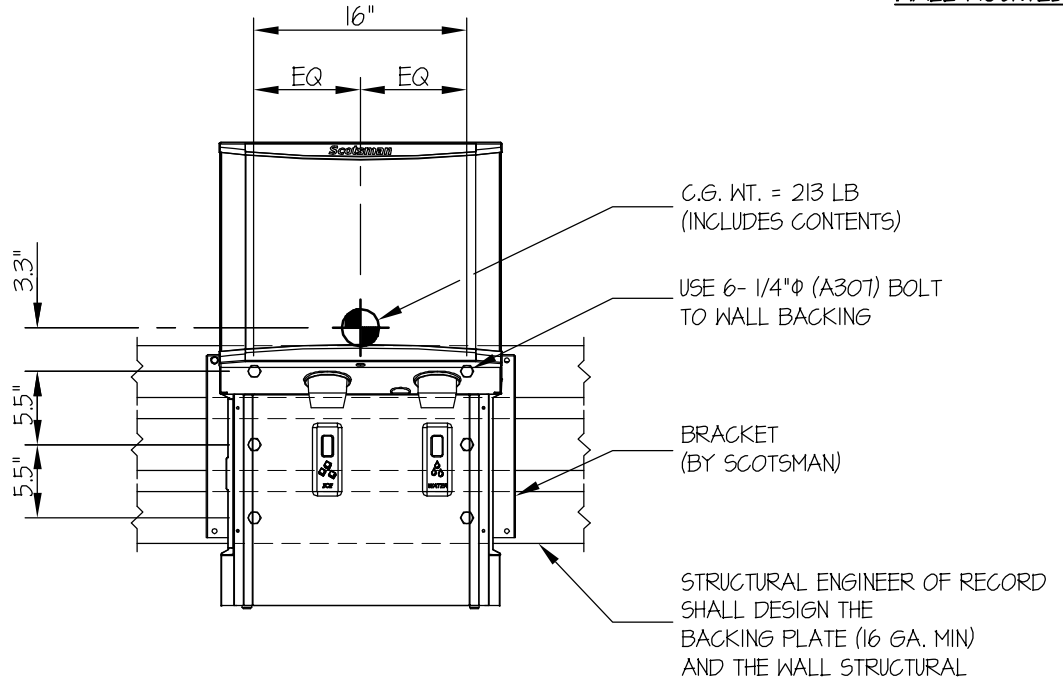
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



$T_u = 586 \text{ LB/BOLT (MAX)}$   
 $V_u = 227 \text{ LB/BOLT (MAX)}$

FRONT ELEVATION

NOTES:

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10 STRENGTH DESIGN IS USED. ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )  
HORIZONTAL FORCE ( $E_h$ ) =  $1.58 W_p$   
VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
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DES. J. ROBERSON

JOB NO. 11-1508

DATE 4/22/15

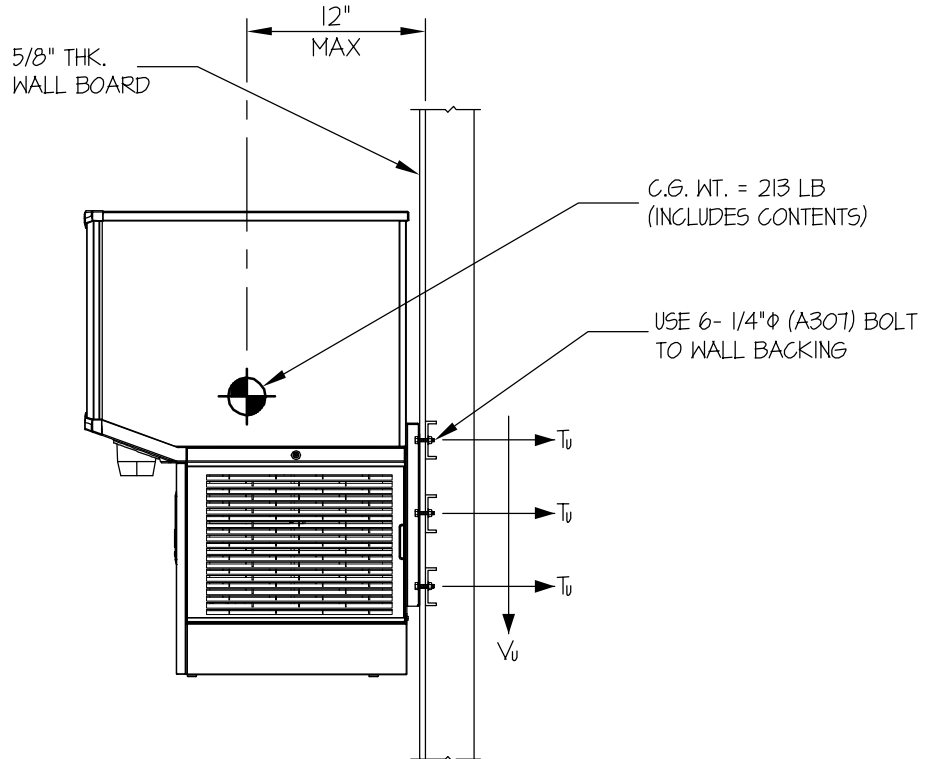
SHEET

2

OF 2 SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



**SIDE ELEVATION**

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED (S<sub>ds</sub> = 2.20, a<sub>p</sub> = 1.0, I<sub>p</sub> = 1.5, R<sub>p</sub> = 2.5, z/h ≤ 1)

WEIGHT = 213 LB

HORIZONTAL FORCE (E<sub>h</sub>) = 1.58W<sub>p</sub> = 337 LB

VERTICAL FORCE (E<sub>v</sub>) = 0.44W<sub>p</sub> = 94 LB

BOLT FORCES:

TENSION (T)

$$T_{U \text{ VERTICAL}} = \frac{(213\#)(12) + 94\#(12'')}{2 \text{ BOLTS } (11'')} = 191 \text{ LB/BOLT}$$

$$T_{U \text{ PARALLEL}} = \frac{337\#(12'')(14.3'')}{1 \text{ BOLT } (16'')(11'')} = 329 \text{ LB/BOLT}$$

$$T_{U \text{ PERP.}} = \frac{337\#(14.3'')}{2 \text{ BOLTS } (11'')} = 219 \text{ LB/BOLT}$$

$$T_{U \text{ MAX}} = 191\# + 329\# + 0.3(219\#) = 586 \text{ LB/BOLT (MAX)}$$

SHEAR (V)

$$V_{U \text{ MAX}} = \sqrt{\left(\frac{(1.2(213\#) + 94\#)}{6 \text{ BOLTS}}\right)^2 + \left(\frac{337\#(14.3'')}{2 \text{ BOLTS } (11'')} \right)^2} = 227 \text{ LB/BOLT (MAX)}$$

BOLT SPEC: 1/4"φ (A307) BOLTS

φT = 1491 LB/BOLT

φV = 807 LB/BOLT



## SCOTSMAN ICE SYSTEM

### HID540 ICE MACHINE (COUNTERTOP MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/13/15**

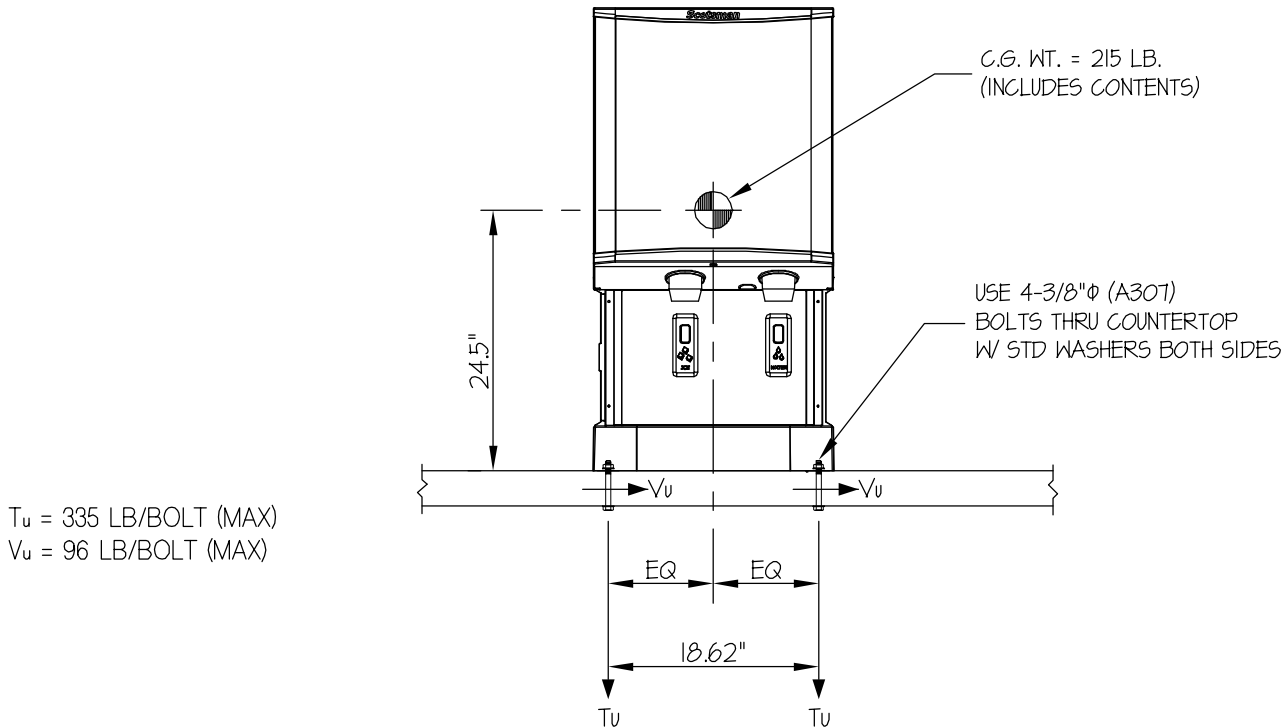
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



$T_u$  = 335 LB/BOLT (MAX)  
 $V_u$  = 96 LB/BOLT (MAX)

**FRONT ELEVATION**

**NOTES:**

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10 STRENGTH DESIGN IS USED. ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )  
HORIZONTAL FORCE ( $E_h$ ) =  $1.58 W_p$   
VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



## SCOTSMAN ICE SYSTEM

### HID540 ICE MACHINE (COUNTERTOP MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/13/15**

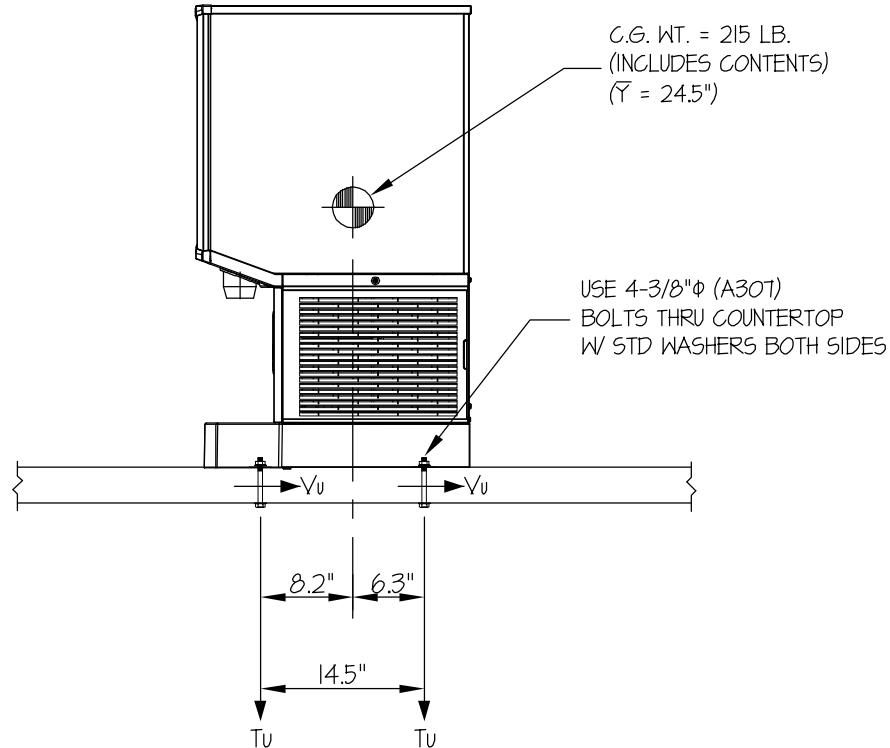
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



**SIDE ELEVATION**

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 215 LB

HORIZONTAL FORCE ( $E_h$ ) =  $1.58W_p = 340$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.44W_p = 95$  LB

BOLT FORCES:

BOLT SPEC: 3/8" phi (A307) BOLTS

$\phi T = 3355$  LB/BOLT

$\phi V = 1723$  LB/BOLT

TENSION (T)

$$T_{U \text{ MAXIMUM}} = \left[ \frac{340\#(24.5'')(8.2'')}{1 \text{ BOLT } (18.62'')(14.5'')} \times (0.3) \right] + \frac{340\#(24.5'')}{2 \text{ BOLTS } (14.5'')} - \frac{(215\#(0.9) - 95\#)(8.2'')}{2 \text{ BOLTS } (14.5'')} = 335 \text{ LB/BOLT (MAX)}$$

( HORIZ - SIDE TO SIDE )                      ( HORIZ - FRONT TO BACK )                      ( 0.9WEIGHT ) -  $E_v$

SHEAR (V)

$$V_{U \text{ MAXIMUM}} = \frac{340\#(8.2'')}{2 \text{ BOLTS } (14.5'')} = 96 \text{ LB/BOLT (MAX)}$$

## SCOTSMAN ICE SYSTEM

### HID540 ICE MACHINE (WALL MOUNTED)

DES. **J. ROBERSON**

JOB NO. **11-1508**

DATE **4/22/15**

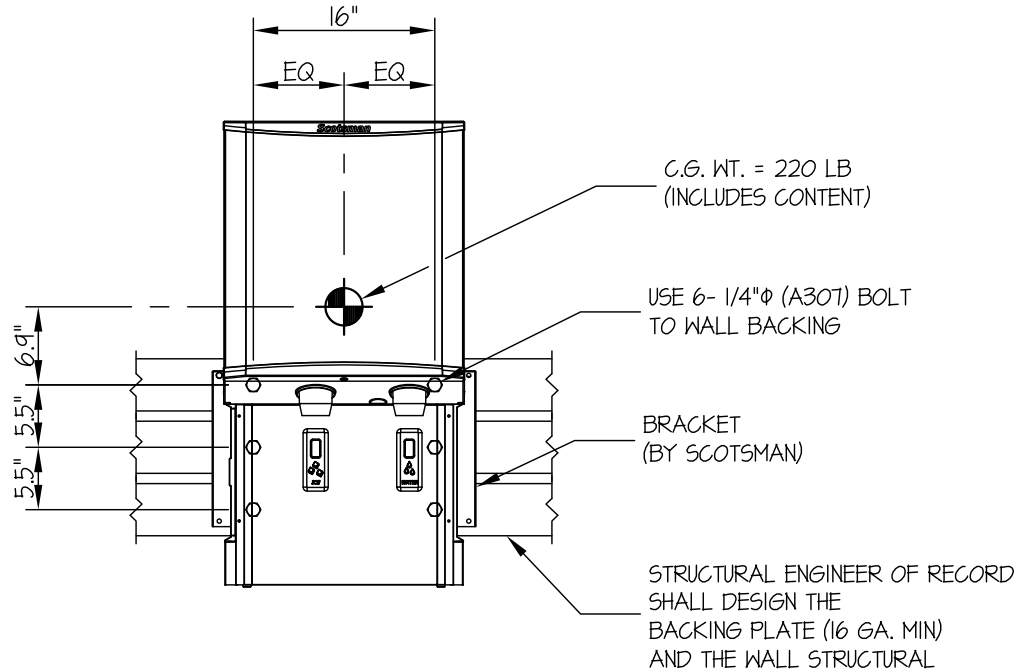
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



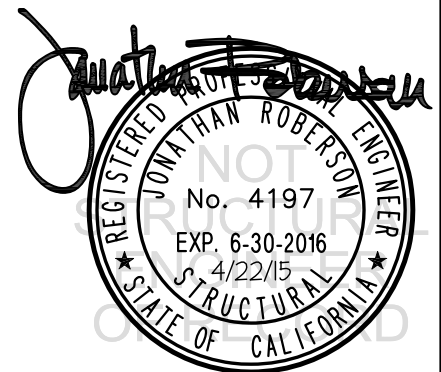
$T_u = 707 \text{ LB/BOLT (MAX)}$

$V_u = 290 \text{ LB/BOLT (MAX)}$

FRONT ELEVATION

NOTES:

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VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$
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## SCOTSMAN ICE SYSTEM

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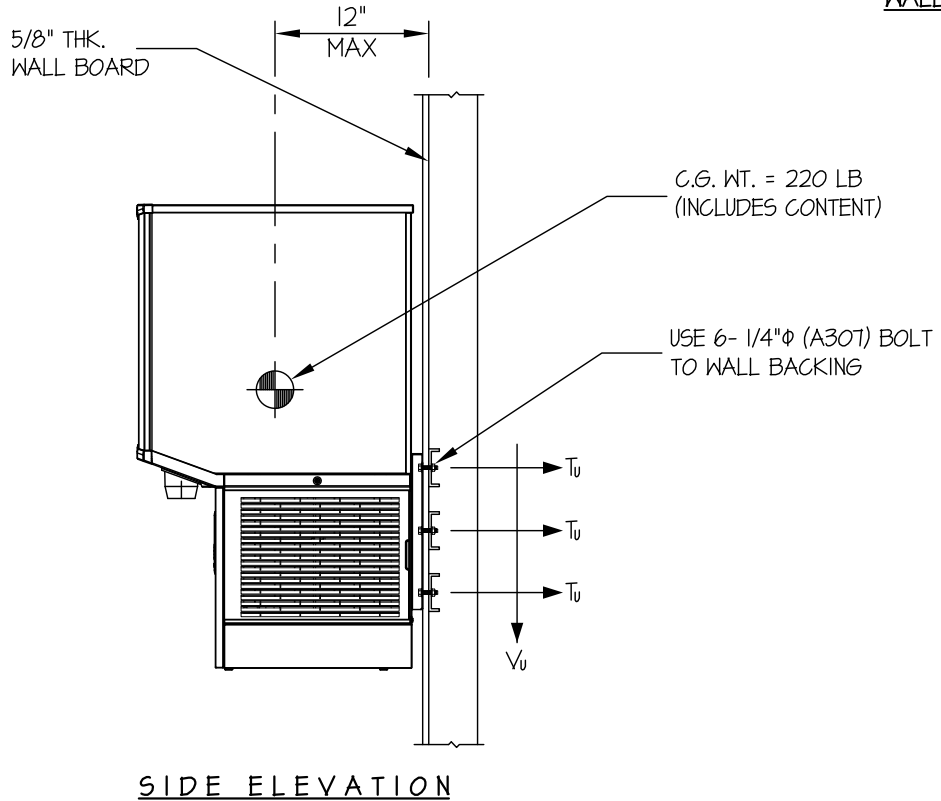
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED ( $S_{ds} = 2.20$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 220 LB

HORIZONTAL FORCE ( $E_h$ ) =  $158W_p = 348$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.44W_p = 97$  LB

BOLT FORCES:

TENSION (T)

$$T_{U \text{ VERTICAL}} = \frac{(220\#)(1.2) + 97\#(12'')}{2 \text{ BOLTS } (11'')} = 197 \text{ LB/BOLT}$$

$$T_{U \text{ PARALLEL}} = \frac{348\#(12'')(17.9'')}{1 \text{ BOLT } (16'')(11'')} = 425 \text{ LB/BOLT}$$

$$T_{U \text{ PERP.}} = \frac{348\#(17.9'')}{2 \text{ BOLTS } (11'')} = 283 \text{ LB/BOLT}$$

$$T_{U \text{ MAX}} = 197\# + 425\# + 0.3(283\#) = 707 \text{ LB/BOLT (MAX)}$$

SHEAR (V)

$$V_{U \text{ MAX}} = \sqrt{\left(\frac{(1.2(220\#) + 97\#)}{6 \text{ BOLTS}}\right)^2 + \left(\frac{348\#(17.9'')}{2 \text{ BOLTS } (11'')} \right)^2} = 290 \text{ LB/BOLT (MAX)}$$

C.G. WT. = 220 LB  
(INCLUDES CONTENT)

USE 6- 1/4"φ (A307) BOLT  
TO WALL BACKING

$T_u$   
 $T_u$   
 $T_u$   
 $V_u$

BOLT SPEC: 1/4"φ (A307) BOLTS

$\phi T = 1491$  LB/BOLT

$\phi V = 766$  LB/BOLT

**SCOTSMAN EQUIPMENT ANCHORAGE**

**MODEL MDT3F12 AND MDT4F12  
ICE DISPENSERS**

DES. R. LA BRIE

JOB 11-0124

DATE 6/20/01

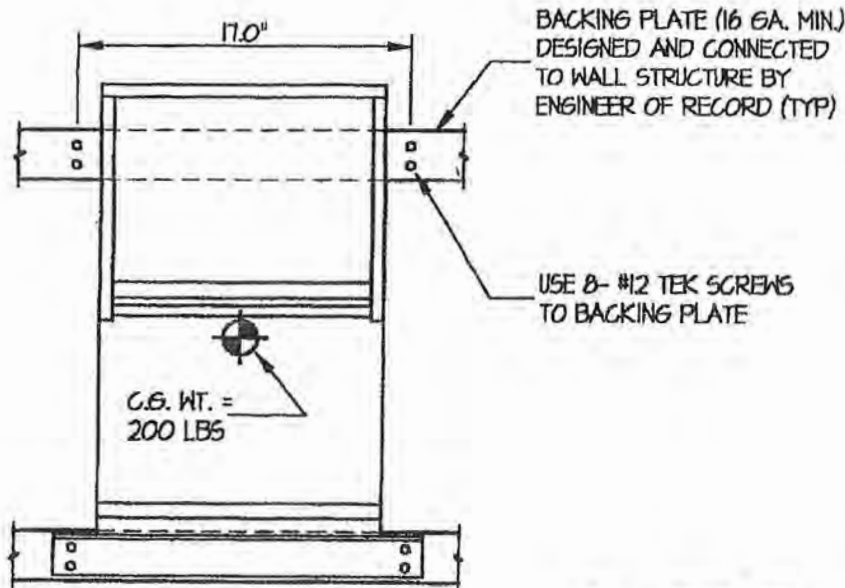
SHEET

**1**

OF 1 SHEET

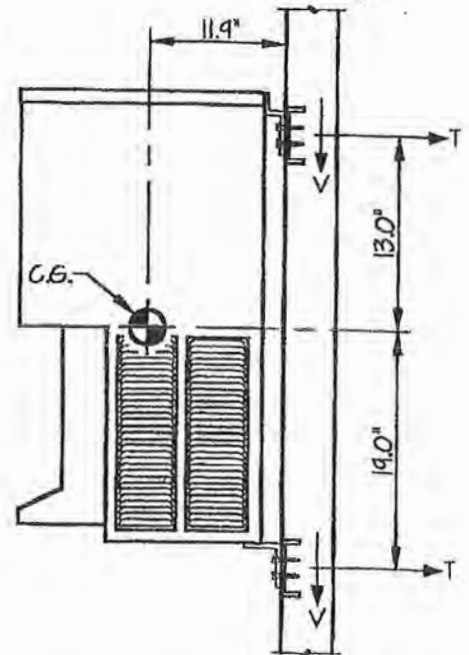
SEISMIC ANCHORAGE

WALL MOUNTED



FRONT ELEVATION

T<sub>MAX</sub> = 48 LBS/BOLT  
V<sub>MAX</sub> = 56 LBS/BOLT



SIDE ELEVATION

LOADS: PER 1998 CALIFORNIA BUILDING CODE - SECTION 1632A

WEIGHT = 200 LBS

HORIZONTAL FORCE (V<sub>H</sub>) = 0.94W = 188 LBS

VERTICAL FORCE (V<sub>V</sub>) = 0.33(V<sub>H</sub>) = 63 LBS

BOLT FORCES:

TENSION (T)

$$T = \frac{188\#}{8 \text{ SCREWS}} + \frac{(200\# + 63\#)11.9\text{'}}{4 \text{ SCREWS } (32.0\text{'})} = 48 \text{ LBS/SCREW (MAX)}$$

SHEAR (V)

$$V = \frac{188\#}{8 \text{ SCREWS}} + \frac{200\# + 63\#}{8 \text{ SCREWS}} = 56 \text{ LBS/SCREW (MAX)}$$



NOTE:

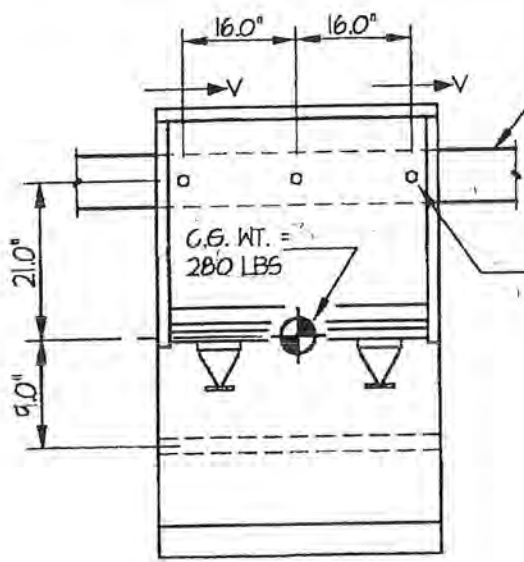
PROVIDE WALL STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN.  
(BY ENGINEER OF RECORD FOR THE BUILDING)

# EASE EQUIPMENT ANCHORAGE & SEISMIC ENGINEERING

<b>SCOTSMAN EQUIPMENT ANCHORAGE</b>  <b>MODEL MDT5N25 ICE SYSTEM</b>	DES. <b>R. LA BRIE</b>	SHEET <b>1</b>  OF 1 SHEET
	JOB <b>11-0124</b>	
	DATE <b>6/20/01</b>	

SEISMIC ANCHORAGE

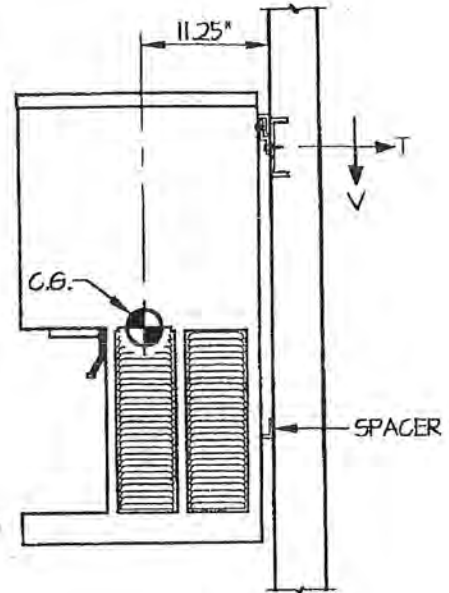
WALL MOUNTED



BACKING PLATE (16 GA. MIN.)  
DESIGNED AND CONNECTED  
TO WALL STRUCTURE BY  
ENGINEER OF RECORD (TYP)

USE 3- #14 TEK SCREWS  
TO BACKING PLATE

**FRONT ELEVATION**



**SIDE ELEVATION**

T<sub>MAX</sub> = 138 LBS/BOLT  
V<sub>MAX</sub> = 245 LBS/BOLT

LOADS: PER 1998 CALIFORNIA BUILDING CODE - SECTION 1632A

WEIGHT = 280 LBS  
HORIZONTAL FORCE (V<sub>H</sub>) = 0.94W = 263 LBS  
VERTICAL FORCE (V<sub>V</sub>) = 0.33(V<sub>H</sub>) = 88 LBS

BOLT FORCES:

TENSION (T)

$$T = \frac{(280\# + 88\#)(11.25\prime\prime)}{3_{\text{SCREWS}}(30.0\prime\prime)} + \frac{263\#(11.25\prime\prime)}{32.0\prime\prime} = 138 \text{ LBS/SCREW (MAX)}$$

SHEAR (V)

$$V = \frac{280\# + 88\#}{3_{\text{SCREWS}}} + \frac{263\#(21.0\prime\prime)}{32\prime\prime} = 245 \text{ LBS/SCREW (MAX)}$$

NOTE:

PROVIDE WALL STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN.  
(BY ENGINEER OF RECORD FOR THE BUILDING)



**SCOTSMAN EQUIPMENT ANCHORAGE**

**MDT5N40 AIR AND WATER NUGGET ICE MAKER/DISPENSER**

DES. R. LA BRIE

JOB 11-0124

DATE 6/20/01

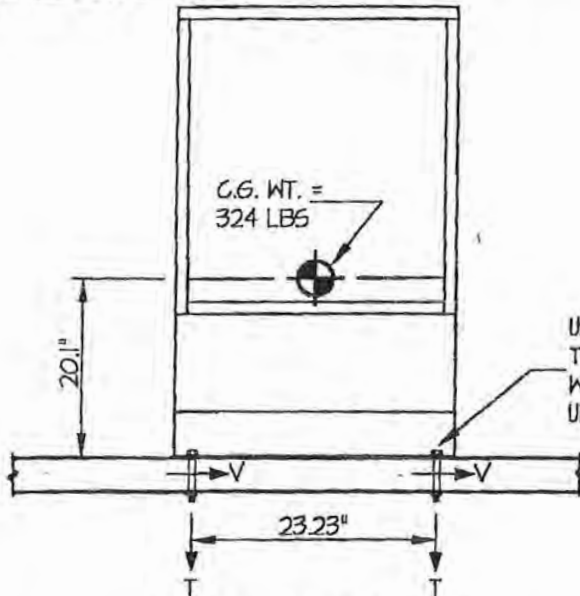
SHEET

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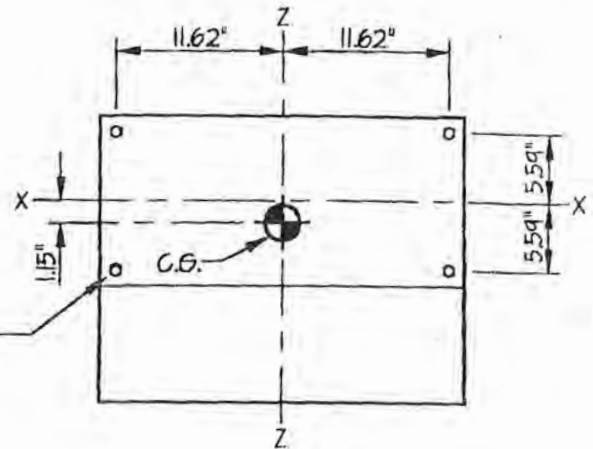
OF 1 SHEET

SEISMIC ANCHORAGE

COUNTERTOP MOUNTED



**FRONT ELEVATION**



**PLAN AT BASE**

T<sub>MAX</sub> = 253 LBS/BOLT  
V<sub>MAX</sub> = 83 LBS/BOLT

**LOADS:** PER 1998 CALIFORNIA BUILDING CODE - SECTION 1632A

WEIGHT = 324 LBS

HORIZONTAL FORCE (V<sub>H</sub>) = 0.94W = 305 LBS

VERTICAL FORCE (V<sub>V</sub>) = 0.33(V<sub>H</sub>) = 102 LBS

**BOLT GROUP PROPERTIES:**

|x-x = 125 in.<sup>4</sup>

|z-z = 540 in.<sup>4</sup>

|y-y = 665 in.<sup>4</sup>

**MOMENTS:**

M<sub>XX</sub> = 305#(20.1") + (324# - 102#)1.15" = 6,386"#"

M<sub>ZZ</sub> = 305#(20.1") = 6,131"#"

M<sub>YY</sub> = 305#(1.15") = 351"#"

**BOLT FORCES:**

TENSION (T)

$$T_{X-AXIS} = \frac{6386" \#(5.59")}{125} - \frac{324\# - 102\#}{4} = 230 \text{ LBS/BOLT}$$

$$T_{Z-AXIS} = \frac{6131" \#(11.62")}{540} - \frac{324\# - 102\#}{4} = 76 \text{ LBS/BOLT}$$

$$T = 230\# + 76\#(0.3) = 253 \text{ LBS/BOLT (MAX)}$$

SHEAR (V)

$$V = \frac{305\#}{4} + \frac{351" \# \sqrt{5.59^2 + 11.62^2}}{665} = 83 \text{ LBS/BOLT (MAX)}$$

**NOTE:**

COUNTERTOP STRUCTURE SHALL BE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN BY OTHERS.



# EASE EQUIPMENT ANCHORAGE & SEISMIC ENGINEERING

## SCOTSMAN EQUIPMENT ANCHORAGE

### MODEL MDT6N90 ICE MAKER

DES. R. LA BRIE

JOB 11-0124

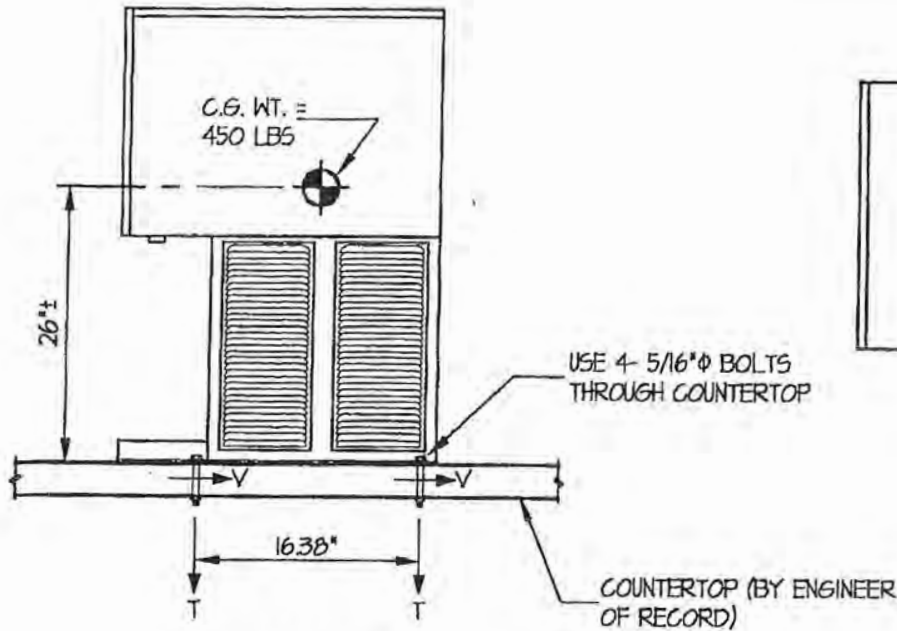
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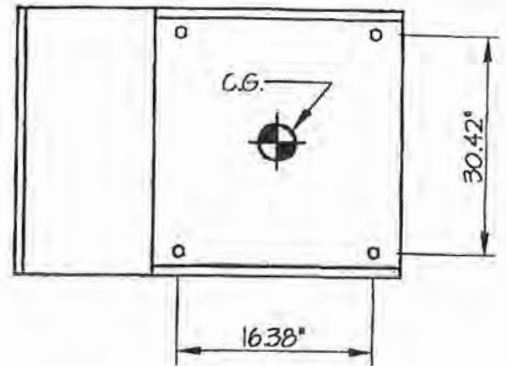
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OF 1 SHEET

#### SEISMIC ANCHORAGE



**SIDE ELEVATION**



**PLAN AT BASE**

T<sub>MAX</sub> = 289 LBS/BOLT  
V<sub>MAX</sub> = 106 LBS/BOLT

LOADS: PER 1998 CALIFORNIA BUILDING CODE - SECTION 1632A

WEIGHT = 450 LBS

HORIZONTAL FORCE (V<sub>H</sub>) = 0.94W = 423 LBS

VERTICAL FORCE (V<sub>V</sub>) = 0.33(V<sub>H</sub>) = 141 LBS

BOLT FORCES:

TENSION (T)

$$T_{\text{SIDE TO SIDE}} = \frac{423\#(26.0'')}{2 \text{ BOLTS}(30.42'')} - \frac{450\# - 141\#}{4 \text{ BOLTS}} = 104 \text{ LBS/BOLT}$$

$$T_{\text{FRONT TO BACK}} = \frac{423\#(26.0'')}{2 \text{ BOLTS}(16.38'')} - \frac{450\# - 141\#}{4 \text{ BOLTS}} = 258 \text{ LBS/BOLT}$$

$$T = 258\# + 104\#(0.3) = 289 \text{ LBS/BOLT (MAX)}$$

SHEAR (V)

$$V = \frac{423\#}{4} = 106 \text{ LBS/BOLT (MAX)}$$

NOTE:

COUNTERTOP STRUCTURE SHALL BE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN BY OTHERS.

